# EXTREME H<sub>2</sub>S REMEDIATION FOR PRODUCED WATER REUSE, IN FRACTURE-STIMULATION

# Tim Underwood Baker Hughes Incorporated

#### ABSTRACT

Hydrofracturing with 100% recycled water is very desirable in highly sensitive clay formations. In the Permian Basin, recycling of produced water can save operators many thousands of dollars per well in fresh water, trucking, and disposal costs. One obstacle to reuse for many produced waters is high hydrogen sulfide ( $H_2S$ ) concentrations.

With typical  $H_2S$  treatments, such as scavengers, vapor recovery, thermal, chemical, and biological oxidation, the cost/bbl is prohibitive on produced water with high  $H_2S$  levels. A new, more economical  $H_2S$  remediation technique recycles  $H_2S$  containing formation water into low suspended solids water. The water is then clarified, creating a low total suspended solids (TSS) solution ready for hydrofracturing.

This paper discusses the treatment of 22,000 bbl of 900 ppm  $H_2S$  produced water used in the successful completion of an 8-stage continuous slickwater frac in the Ramsey formation, of the Black River South field, in Eddy County, New Mexico.

#### **INTRODUCTION**

In the Permian Basin, recycling of produced water can save operators many thousands of dollars per well in fresh water, trucking, and disposal costs. Hydrofracturing with 100% recycled water is also very desirable in highly sensitive clay formations.

One obstacle to reuse for many produced waters is high hydrogen sulfide ( $H_2S$ ) concentrations. The corrosive and toxic nature of  $H_2S$  necessitates its removal. With many fields containing more sour water, more operators are looking for ways to recycle produced water containing significant levels of  $H_2S$ .

A New Mexico operator needed to complete wells in a formation that was extremely sensitive to clay swelling. The operator wanted to maintain the formation permeability by reusing produced water to minimize swelling.

Unfortunately, the produced water from wells in this area also have high levels of  $H_2S$ . If the operator couldn't reuse the water, an alternative and more expensive gas fracturing completion would have to be used. The operator called for recommendations after they had collected and stored nearly 25,000 bbl of produced water containing more than 900 ppm  $H_2S$  for fracturing.

The cost of mitigating such high levels of  $H_2S$  safely was a primary challenge. Traditional oilfield  $H_2S$  treatments cost more than USD 10 per barrel to treat this level of  $H_2S$ . After researching alternatives, the recommended solution was treatment with hydrogen peroxide ( $H_2O_2$ ) oxidation to remove  $H_2S$  and maintain the water quality required to make up fracturing fluid.

Lab, pilot, and full scale treatments were performed on waters with  $H_2S$  concentrations ranging from 600 to 900 ppm. Results of treating 49 frac tanks filled with high  $H_2S$  water demonstrate the safe economical use of  $H_2O_2$  for eliminating  $H_2S$ , while maintaining the formation water quality required for fracturing fluid makeup.

#### **PROBLEM SOLUTION**

Technologies to remove  $H_2S$  from water include treatments such as scavengers, vapor recovery, thermal, chemical, and biological oxidation. To assist in selecting an appropriate remediation technique, the following  $H_2S$  removal processes were candidates screened using Quality Function Deployment (QFD) methodology:

- Zinc Oxidation
- Thermal Oxidation

- Bacterial Oxidation
- Vapor Recovery

• Chlorine Dioxide

• H<sub>2</sub>S Scavenger Chemicals

Hydrogen Peroxide Oxidation

The QFD filtered out the following four processes as the best fit for customer needs (Table 1): Chlorine Dioxide, Vapor Recovery, Acrolein Scavenger, and Hydrogen Peroxide Oxidation. These final four processes are primarily chemical applications.

The pricing for these methods was determined from previous field experience and lab testing estimates on the  $H_2O_2$  process (Table 1). The first three, more common oil industry methods have various degrees of efficiency and removal efficacy, but are cost prohibitive for reuse of produced water with high  $H_2S$  levels. With the QFD results and pricing considerations, the  $H_2O_2$  oxidation method was advanced for further testing.

## Lab Tests

Lab testing with  $H_2O_2$  was performed to determine dosages and reaction time required to oxidize the  $H_2S$  to levels required to prevent excessive off-gas from reaction tanks. Tests at different dosages demonstrated which preferred ppm of active  $H_2O_2$  for every ppm of  $H_2S$  would eliminate lead acetate detectable dissolved  $H_2S$  in less than 30 minutes at room temperature.

#### Full Scale Field Treatment Process

A 500 bbl pilot treatment was set up to inject  $H_2O_2$  into the  $H_2S$  water. Following the successful replication of lab findings in the one tank pilot test, the customer's 49 tanks of high  $H_2S$  produced water were treated using the same treatment technique.

#### H<sub>2</sub>S and Hydrogen Peroxide - Health and Safety Considerations

Treating produced water containing high  $H_2S$  levels with  $H_2O_2$  poses other operational safety factors which need to be considered. High  $H_2S$  levels in the raw water pose off-gas safety concerns, and additional monitoring is needed. To address these additional hazards, the following strategies were utilized:

- Monitoring general work area and reaction tank H<sub>2</sub>S levels with strategic placement of multiple H<sub>2</sub>S and 4gas monitors reporting to a central monitoring station
- Utilizing audible and visible alerts with NIOSH H<sub>2</sub>S limit set points
- Use of standby rescue technicians, air trailer, and SCBA equipment

Concentrated  $H_2O_2$  in contact with hydrocarbons under the right conditions could generate enough heat to promote combustion. Produced water generally has too low hydrocarbon content to give any appreciable reaction temperature increase.

#### **RESULTS**

## Targeted Finished Water Parameters Treatment Results

The primary finished water parameters of concern during the treatment were  $H_2S$ , water clarity,  $H_2O_2$  residual, friction loop performance, and frac fluid performance. As tested during treatment, in the attached analyses, and demonstrated by sand placement during the fracture:

- H<sub>2</sub>S levels were reduced to zero after 30 minutes reaction time in all 49 tanks processed
- Final clarity was below 80 FTU with rapid clarification and below 30 FTU using overnight settling clarification
- $H_2O_2$  residuals drop from 100 ppm during treatment to zero after eight hours (Table 2)
- Friction loop results showed the 50% reduction achieved with typical FR addition rates (Figure 1)
- Designed quantity of proppant was placed with 5 gpt and 1 gpt slick water treatments

#### Peroxide Residual

Preliminary hydration tests using  $H_2O_2$  treated water samples show that  $H_2O_2$  residuals in the 25-100 ppm range do not interfere with hydration of polymers. Friction loop testing was done on post- $H_2O_2$  treated water with no  $H_2O_2$ 

residual (Figure 1), but further testing is needed for friction reduction performance at various levels of residual. Until the levels of tolerable residual for various linear and cross-linked polymers are known, one of the goals of field treatment should be to keep  $H_2O_2$  dosages at the minimum required for  $H_2S$  removal.  $H_2O_2$  neutralizers could also be kept on hand for application if  $H_2O_2$  is overdosed.

Increased Sulfate Concentration in Treated Water

Another parameter that was considered is the increase in sulfate concentration in the finished water due to sulfide oxidation. In neutral-to-alkaline conditions, the two following reactions take place:

- 1. Reaction which predominates closer to neutral pH:  $H_2S + H_2O_2 \rightarrow S_0 + 2H_2O$
- 2. Reaction which predominates at pH 9:  $S^{2-} + 4H_2O_2 \rightarrow SO_4^{=} + 4H_2O$

In the treatment of the  $H_2S$  water during this project, the sulfate concentration rose from 2111 ppm in the raw water to an average of 2550 ppm in the treated water. Sulfate increases were entered into scale modeling software to assist with prediction of sulfate scaling problems. The 400 ppm increase in sulfates at this treatment was not problematic, but is a factor which should be monitored and modeled for each different treatment. The remainder of the oxidized sulfur is precipitated and removed during clarification.

#### **SUMMARY**

Use of the peroxide oxidation process for remediation of high (900) ppm  $H_2S$  produced water has been demonstrated for 100% recycling into hydrofracturing fluid. The 24,000 bbl treatment demonstrated the  $H_2O_2$  remediation technique can economically recycle  $H_2S$  containing produced water into low suspended solids water, while maintaining the formation water quality required for fracturing fluid makeup. In many formations containing sensitive clays, the cost of required levels of KCl alone, to make fresh water useable, is more costly than treatment and recycling of formation's own produced water. (Table 3)

Safe operating procedures with high  $H_2S$  water were successfully implemented to mitigate the risk of exposure to  $H_2S$  off-gas. With the demonstrated success of  $H_2O_2$  oxidation in lowering costs for recycling  $H_2S$  containing produced water, operators can now save many thousands of dollars per well with this treatment.

## Table 1

Estimated cost of various processes to remove 1000 ppm  $H_2S$  from produced water.

H <sub>2</sub> S Removal Process	Estimated Cost per BBL, to treat 1000ppm H <sub>2</sub> S Water
Chlorine Dioxide	>\$10.00
Vapor Recovery	\$6.50
Acrolein	\$12.60
H <sub>2</sub> O <sub>2</sub>	\$6.00

$H_2O_2$ Residual vs. Time										
Time After H <sub>2</sub> S Eliminated	Residual [H <sub>2</sub> O <sub>2</sub> ] ppm									
30 Minutes	100+									
6 Hours	8									
24 Hours	0									

#### Table 3

# Cost of Various External Sources of Fracturing Water, Verses Re-Use of Formation's Own Water

Hauling a	and Dispo	sal Costs p	oer BBL	for SWD I	Disposal of	Fluid, (not	t recycled for	fracturing)		\$/bbl
	Disposal c	cost at Operator Owned SWD, for water not recycled to frac								<.25
	Disposal c	cost at commercial SWD, for water not recycled to frac								.5-2.5
	Hauling	\$1/bbl/hr or .5-1.00/bbl Texas, \$4.00-\$8.00/bbl PA							.50-8.00	
	Hauling and disposal costs, Rick McCurdy, Chesapeake Energy, "Underground Injection Wells for Produced Water Disposal"									
Fresh W	ater Costs									
	Purchase Fresh Water		(2012-201	(2012-2013 Price ranges in Permian)					0.15-2.5	
	Hauling	\$1/bbl/hr o	or (\$.5-\$1	00/bbl in	Texas) (\$4.00	0-\$8.00/bbl	in PA)			.50-8.00
PURCHAS	ED FRESH V	NATER COS	<u>TS:</u>							
Cost/BBL	Example U	Jsing Purch	ased & T	ransporte	d Fresh Wate	er at only \$.	50/BBL Fresh W	/ater Cost		
	Produced	water dispo	sal (since	not used)	at Operator	Owned SWI	D, (.25 Disp + 1.	75 Transport to	Disposal)	2.00
	Purchase F	resh Water	<sup>.</sup> at \$.50 p	per bbl						0.50
	Hauling of	Purchased	Fresh Wa	ter						0.75
	KCI	\$3.50 Min for 2% KCl						3.50		
	*Model Assumes no cost for risk of formation damage, from synthetic KCl water									
										6.75
Example	Cost/BBL	Approx C	ustome	r Cost, fo	r H2PROHD	Treated V	Nater (40,000	bbl treatmer	nt <u>)</u>	
	Customer cost per BBL for a 40K bbl treatment of 700 ppm H2S, already in holding tanks							4-5.00		
	Customer cost per BBL for a 40K bbl treatment of 200 ppm H2S, already in holding tanks								3-4.00	
		Customer cost per BBL for a 40K bbl treatment of 1000 ppm H2S, as produced							3-5.00	
		Customer cost per BBL for a 40K bbl treatment of 200 ppm H2S, as produced							1.25-2.00	



Friction Pressure Reduction of MaxPerm 20A Slickwater

Figure 1